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## EVALUATING FIRE PERFORMANCE OF NAIL-LAMINATED TIMBER: SURFACE FLAMMABILITY

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#### EVALUATING FIRE PERFORMANCE OF NAIL LAMINATED REVIEWER TIMBER: SURFACE FLAMMABILITY

PROJECT NO. 301013024

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## 1. BACKGROUND

Nail-laminated timber (NLT) is a mass timber product that has historically been used in industrial and commercial heavy timber buildings in Canada. There is interest to expand the use of this product into modern larger and taller wood buildings, which has been demonstrated by the recent release of the Canadian [1] and American [2] NLT design guides. NLT is simple to construct, uses a large volume of low-grade lumber, and is as cost competitive as other prefabricated mass timber elements. It is commonly used in the construction of floors; although not commonly used for walls, it can be used in the construction of vertical shafts, such as for elevators or exit stairs.

NLT is recognized as solid wood construction in the National Building Code of Canada (NBCC) [3] under Appendix D-2.4; however, significant knowledge gaps exist related to its overall fire performance. The basis for the assigned fire resistance ratings for solid wood assemblies in the NBCC is unknown; therefore, there is a need to provide technical and scientific data to support the fire safe design of these mass timber assemblies. Similarly, flame spread rating (FSR) data is available for various wood species, but there is no known data for NLT assemblies specifically. Performance data and technical information needs to be generated so that designers have the tools to gain approvals, which will ultimately lead to greater adoption of mass timber construction.

## 2. OBJECTIVE

The objective of this project is to establish fundamental fire performance data for the design and specification of NLT assemblies; this project specially addresses determining FSRs for NLT. The goal of this project is to confirm that NLT, when used as a mass timber element, has a lower FSR than standard thickness SPF boards when tested individually and flatwise. The project also considers how the surface profiles, design details, and the direction of an assembly might influence flame spread. This includes the evaluation of typical architectural features, such as a 'fluted' profile.

Having this technical information will support project approvals for the use of NLT elements in larger and taller wood buildings, as well as provide scientific justification for Authorities Having Jurisdiction (AHJ) to review and accept this construction method. This research will provide the evidence for designers to demonstrate their design have met or exceeded fire safety requirements. Ultimately the intent is to expand the adoption of manufactured solid timber construction for larger and taller buildings, as well as for non-traditional wood markets (such as institutional or commercial buildings).

Other aspects of this project (in separate reports) include evaluating fire resistance of NLT [4], and assessing how NLT charring rates might be affected by gaps between boards [5].

## **3. TECHNICAL TEAM**

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## 4. INTRODUCTION

The NLT Design & Construction Guides [2] [3] provide comprehensive information on the design of NLT, however little detail is given related to the fire performance of this product. This is due to a lack of available fire test data for NLT assemblies. FPInnovations has previously evaluated the fire resistance of a screw laminated timber-concrete composite (TCC) floor [6], but little to no other data is available.

Having comprehensive data to confirm the overall fire performance of wood assemblies is key to understanding how to appropriately design them, this includes both fire resistance and flame spread data. Flame spread across the surface of wood assemblies is an important property to evaluate since the NBCC limits the amount of exposed combustible interior finishes based on their FSR, when evaluated in accordance with CAN/ULC-S102 [7]. In some situations, according to the NBCC, exposed wood wall and ceiling elements can have a FSR of up to 150 in sprinklered buildings, Table 3.1.13.2 [3], with limitations on surface area coverage. The FSR for vertical service spaces (such as elevator hoistways) and exits is 25. In high-rise buildings, as defined in the NBCC, the Smoke Developed Classification (SDC) may also be limited. The SDC is evaluated during the FSR test procedure.

The NBCC assigns FSR of 150 to typical wood products in Section D-3 of Division B, including lumber with a minimum thickness of 16 mm and various plywoods. FSR data for 19 mm lumber of different species is available in Fire Safety Design in Buildings [8]; the FSR for SPF products ranges from 65-230.

FPInnovations has evaluated flame spread on other mass timber assemblies and found that mass timber products exhibit low FSRs compared to traditional lumber, due to their thickness [9]. Table 1 provides a summary of the FSRs for these mass timber products.

	Thickness	FSR	SDC
3-ply CLT			
E1 SPF Stress Grade	105 mm	35	40
V2 SPF Stress Grade	99 mm	40	30
3-ply CLT E1 SPF Stress Grade	105 mm	25	20
with intumescent coating	105 mm	25	20
Parallel Strand Lumber (PSL)	89 mm	35	25
Laminated Strand Lumber (LSL)	89 mm	75	85

## 5. PROCEDURE

Flame spread tests were conducted in accordance with CAN/ULC-S102 [7] to establish the FSR of NLT. The standard requires three replicate tests be conducted for each assembly.

The SPF NLT samples were prepared and conditioned at the FPInnovations laboratory in Vancouver; testing was completed by Intertek Testing Services in Coquitlam. Assemblies were tested on June 26<sup>th</sup> and September 25<sup>th</sup>, 2018.

Flame spread was evaluated for NLT with lumber boards parallel to the longitudinal direction of the CAN/ULC-S102 testing tunnel. Further testing was conducted to also assess how surface profiles, design details, and the direction of an NLT assembly influences flame spread. The four sections that were evaluated are:

- A Standard NLT parallel to tunnel
- B Standard NLT perpendicular to tunnel
- C Fluted profile, parallel to tunnel
- D Fluted profile, perpendicular to tunnel

The fluted profile was a simple alternating staggered depth cross-section using nominal 2x4s and 2x6s. Typcial NLT and the fluted profile are shown in Figure 1.



Standard NLT



Fluted NLT

Each of the specimens was constructed in 1830 mm (6') sections; four sections were placed end-to-end in the tunnel to reach a total length of 7315 mm (24'). The NLT was constructed using 3" smooth shank galvanized nails. One row of nails was staggered at 180 mm (7") o.c., placed 20 mm from the bottom and top edge. SPF No. 2 grade lumber was used.

#### 5.1 Designs

#### 5.1.1 Standard NLT – Parallel (A)

The standard NLT (A) assemblies were constructed using nominal 2x6" lumber with the length of the boards running parallel to the tunnel. Each section was 610 mm (24") wide (16 boards across), as shown in Figure 2. Figure 3 shows constructed sections of the constructed A assemblies, which demonstrate how natural imperfections in boards affect the finished surface.



Figure 2. Assembly A configuration

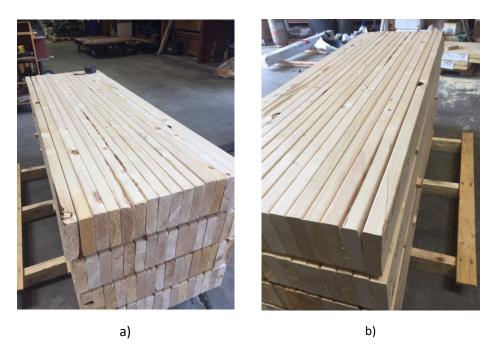


Figure 3. Constructed A panels

#### 5.1.2 Standard NLT – Perpendicular (B)

The standard NLT – perpendicular (B) assemblies were constructed using nominal 2x6" lumber with the length of the boards running perpendicular to the tunnel. Each section was 585 mm (23") wide. Boards were cut to 508 mm (20") and nailed together with boards added to either side along the length of each section to stiffen the assembly. The assembly configuration is shown in Figure 4 and completed assemblies are shown in Figure 5.

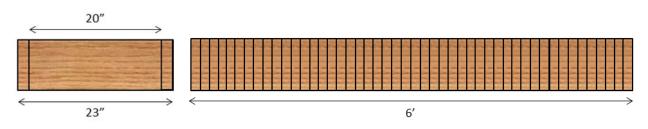


Figure 4. Assembly B configuration



Figure 5. Constructed B panels

#### 5.1.3 Fluted NLT – Parallel (C)

The fluted NLT – parallel (C) assemblies were constructed using alternating nominal 2x4" and 2x6" lumber with the length of the boards running parallel to the tunnel. The two outermost boards were 2x6s to ensure adequate support along the wall of the tunnel. Each section was 570 mm (22.5") wide (15 boards across). The assembly configuration is shown in Figure 6 and constructed panels are shown in Figure 7.



2.5

6' Figure 6. Assembly C configuration



Figure 7. Constructed C panels

#### 5.1.4 Fluted NLT – Perpendicular (D)

The fluted NLT – perpendicular (D) assemblies were constructed using alternating nominal 2x4" and 2x6" lumber with the length of the boards running perpendicular to the tunnel. Each section was 585 mm (23") wide. Boards were cut to 508 mm (20") with boards added to either side to stiffen assembly. The configuration is shown in Figure 8 and constructed panels are shown in Figure 9.

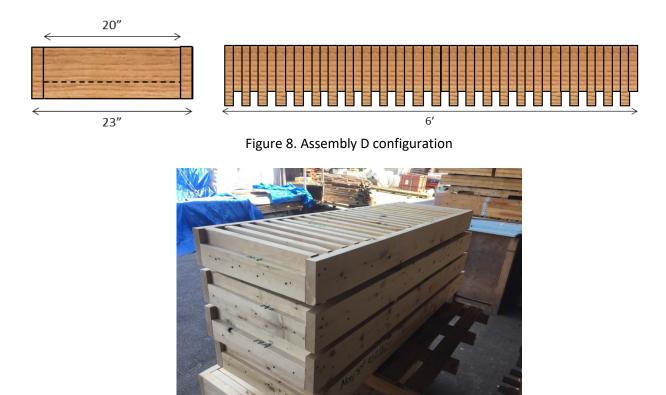


Figure 9. Constructed D panels

#### 5.2 Conditioning

The specimens were conditioned at  $23 \pm 3^{\circ}$ C and  $50 \pm 5\%$  RH prior to testing, in accordance with CAN/ULC-S102, which would provide a wood equilibrium moisture content of approximately 9%. For hygroscopic materials, such as wood, the standard indicates that a constant mass is deemed to be achieved for the samples when mass change over 72 hours is less than 1%.

For hygroscopic materials the moisture content must be taken immediately prior to the test. Average moisture content readings are given for each of the samples in Table 2. Readings were taken using a Delmhorst RDM-3 pin meter set to SPF.

Sample	Average MC (%)
A1	10.0
A2	10.4
A3	9.2
B1	9.1
B2	8.9
B3	9.0
C1	9.3
C2	11.5
C3	9.4
D1	9.4
D2	10.8
D3	9.5

## 6. **RESULTS**

A summary of the results from the flame spread tests is given in Table 3. The official flame spread reports are included as Appendices to this report.

	Flame Spread Rating	Smoke Developed Classification
NLT Parallel to tunnel (A)	50	40
NLT Perpendicular to tunnel (B)	45	55
NLT Fluted Parallel to tunnel (C)	91	105
NLT Fluted Perpendicular to tunnel (D)	65	125

Table 3. Summary	of Flame Spread Results
rubic 5. Summary	or riunic opredu Results

#### 6.1 A – NLT Parallel

The results for the standard NLT parallel to the tunnel (A) are given in Table 4. There was some variability in the results, for example the A3 flame spread result was higher than the other two replicates. The tests were completed on different days, with the tunnel being calibrated before each series of tests. Pictures before, during and after the test are shown in Figure 10.

Table	4.	А	Results
		•••	

Run	Flame Spread	Flame Spread Rating	Smoke Developed	Smoked Developed Classification
A1	40		19	
A2	45	50	50	40
A3	69		53	

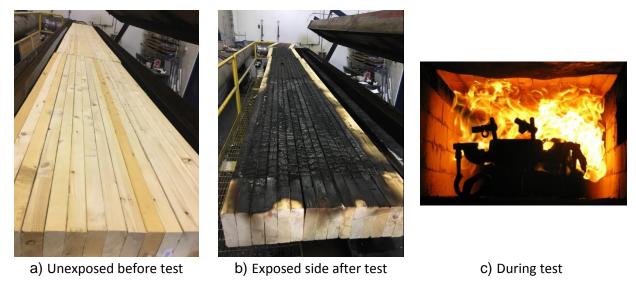


Figure 10. NLT Parallel (A) - Before and After Test

#### 6.2 B – NLT Parallel

The results for the standard NLT perpendicular to the tunnel (B) are given in Table 5. Pictures before, during and after the test are shown in Figure 11.

Table	5.	В	Results

Run	Flame Spread	Flame Spread Rating	Smoke Developed	Smoked Developed Classification
B1	35		72	
B2	47*	45	*	55
B3	55		40	

\*Due to a program error data was not collected. FSR result manually calculated.

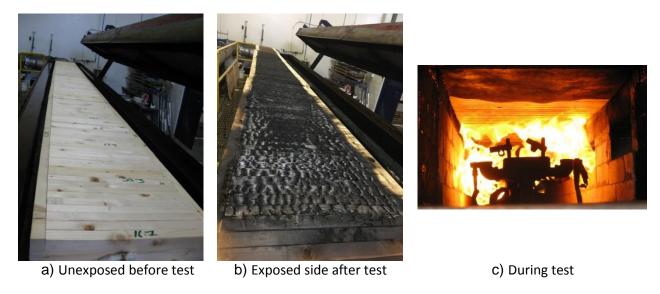


Figure 11. NLT Perpendicular (B) - Before and After Test

#### 6.3 C – NLT Fluted Parallel

The results for the fluted NLT parallel to the tunnel (C) are given in Table 6. Pictures before, during and after the test are shown in Figure 12. The smoke developed measurement was lower in test C1 than the other two replicates.

Run	Flame Spread	Flame Spread Rating	Smoke Developed	Smoked Developed Classification
C1	90		67	
C2	84	91	153	105
C3	99		100	



Figure 12. Fluted NLT Parallel (C) - Before and After Test

#### 6.4 D – NLT Fluted Perpendicular

The results for the fluted NLT perpendicular to the tunnel (D) are given in Table 7. There is some variability in the results. The samples were tested on different days; the tunnel was calibrated before series was completed. Pictures before, during and after the test are shown in Figure 13.

Table	7	п	Results
rable	7.	υ	nesuits

Run	Flame Spread	Flame Spread Rating	Smoke Developed	Smoked Developed Classification
D1	53		186	
D2	100	65	49	125
D3	48		147	

The second assembly (D2) tested had a much higher flame spread than the other two replicates, which increased the overall FSR. This sample ignited within a similar timeframe to the others, 28 s. The flame reached the end of the tunnel in 218 s, whereas the others approached the end of the tunnel at the end of the test (600 s). It is not clear why this sample had a higher flame spread. The results for the other two runs were consistent with the values observed for assemblies A and B.



Figure 13. Fluted NLT Perpendicular (D) - Before and After Test

## 7. DISCUSSION

#### 7.1 Effects of Surface Profile

The FSR for typical flat NLT was found to be 50 and 45, whether it was oriented parallel to the tunnel or perpendicular, respectively. The similarity in these numbers demonstrates that the difference in orientation had little impact on the overall FSR. Despite the chamfer of the boards and naturally uneven surface of NLT that results during construction, the face can be considered to be essentially smooth in either direction for the purposes of flame spread evaluation. Figure 14 illustrates the typical surface profile for NLT (assembly A). These numbers are also consistent with other mass timber products with FSRs of 35-40, but slightly higher. As expected, the FSR of NLT is lower than typical flatwise SPF lumber species, assigned a value of 150 in the NBCC.



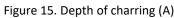
Figure 14. NLT surface profile (A)

The FSRs for the fluted profiles were higher than the standard NLT panels, reaching 91 and 65 for the parallel and perpendicular orientations respectively. This indicates that varied depth surface profiles have an impact on FSRs. For fluted profiles, there is an increased exposed surface area which can result in more contribution of wood to a fire. Within the flutes, heat can be radiated between opposite surfaces and trapped between the flutes, unable to easily dissipate, thus promoting increased burning. When flutes are used, there is a greater difference between FSRs depending on the orientation of the boards. In this case, the flutes parallel to the tunnel resulted in higher FSRs.

#### 7.2 Charring Between Boards

The depth of charring along the surface was less than 1 mm, as shown in Figure 15, for the second section from the burner location (A assembly).





Looking between boards following the tests it could be seen that the exposed surface of the wood charred a few millimetres, but further into the gaps between boards the wood was uncharred, shown in Figure 16. This may be a result of a lack of oxygen in the narrow spaces between boards, preventing combustion from occurring up into the gaps. This may have implications on charring rates in evaluating fire resistance of these assemblies.



Figure 16. Depth of char between boards in first panel (A assembly)

For the fluted perpendicular profile, there were areas of uncharred wood in the inside corners of the flutes, which was more prominent at the boards near the end of the tunnel. Figure 17 shows the charring between the flutes for the perpendicular orientation at different locations. Near the end of the tunnel, the flame front progressed before all of the wood within the flute was involved in fire.

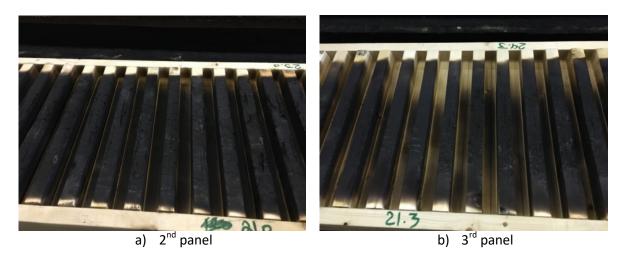


Figure 17. D. Charring between flutes

#### 7.3 Extinguishment

At the end of the flame spread tests a hose is used to extinguish the fire. There were instances of residual burning in some gaps between boards after hose application, such as is shown in Figure 18. This represents a potential challenge for fire fighters to extinguish fires in NLT assemblies. This was also an issue for the fluted perpendicular assemblies, where the flutes shielded the flute cavities, making it difficult to put water on areas that were still burning.

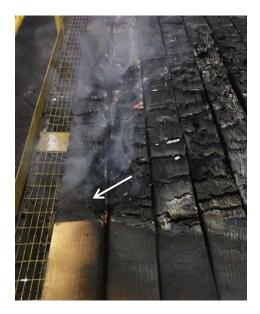


Figure 18. Burning between NLT boards (A assembly)

## 8. CONCLUSION

Flame spread testing was conducted on NLT profiles to establish FSRs. Four configurations of assemblies were evaluated: standard NLT with boards parallel to the tunnel (A), standard NLT with boards perpendicular to the tunnel (B), a simple staggered depth (fluted) profile with boards parallel to the tunnel (C), and a fluted profile with boards perpendicular to the tunnel (D). The test results are given in Table 8. The two standard NLT assemblies had similar FSRs of 50 and 45, for parallel and perpendicular, respectively. The orientation of the standard NLT did not have a significant impact on the FSR. These values are consistent, but are slightly higher than FSRs other mass timber assemblies.

The fluted profiles received higher FSRs which may be in part due to a greater exposed surface area of wood. The fluted profile parallel to the tunnel had the highest FSR of 91, and the perpendicular orientation received a FSR of 65. For this profile, the orientation had a greater impact on FSR.

	Flame Spread Rating	Smoke Developed Classification
NLT Parallel to tunnel (A)	50	40
NLT Perpendicular to tunnel (B)	45	55
NLT Fluted Parallel to tunnel (C)	91	105
NLT Fluted Perpendicular to tunnel (D)	65	125

Table 8. Flame Spread Results

Examining the assemblies after the test, it could be seen that the surface was charred, however in some larger gaps the charring did not extend up between boards. This may be a result of a lack of oxygen in the narrow spaces between boards, preventing combustion from occurring up into the gaps and may have implications for charring rates in evaluating fire resistance of NLT.

Instances of residual burning after the tests within some gaps were noted. This represents a potential issue for extinguishment as these areas may be difficult to readily detect or target with a hose. The fluted profile also posed challenges to extinguish since the flutes shield the cavities; extinguishing a fire on a fluted surface may be challenging depending on the direction of water application.

## 9. **REFERENCES**

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## Appendix I: NLT Parallel to Tunnel (A) Testing Report



# FP INNOVATIONS TEST REPORT

REPORT ISSUED TO FP Innovations 580 Booth Street Ottawa, ON K1A 0E4 CAN SCOPE OF WORK

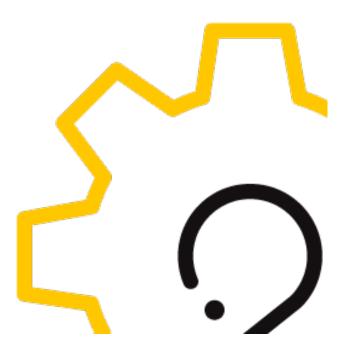
Report of R&D testing nominal 2 in. by 6 in. SPF NLT Panels (Parallel) for compliance with the applicable requirements of the following criteria: CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

## REPORT NUMBER

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**TEST REPORT FOR FP INNOVATIONS** 

REPORT NO.: G103546754 **REVISION DATE: OCTOBER 19, 2018** 

#### CONCLUSION

The samples of nominal 2 in. by 6 in. SPF NLT Panels (Parallel) submitted by FP Innovations, were tested in accordance with CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

The product test results are presented in Section 7 of this report.

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Thile Greg Philp

REVIEWER **BUILDING PRODUCTS CANADA** 

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#### **TEST REPORT FOR FP INNOVATIONS** Revised October 19, 2018

#### **SECTION 1**

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#### **SECTION 2**

#### OBJECTIVE

Intertek Testing Services NA Ltd. (Intertek) has conducted testing for FP Innovations to evaluate the surface burning characteristics of 2 in. by 6 in. SPF NLT Panels (Parallel). Testing was conducted in accordance with the standard methods of CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

This evaluation began June 26, 2018 and was completed September 25, 2018.

#### SECTION 3

#### SAMPLE SELECTION

Samples were submitted to Intertek directly from the client and were not independently selected for testing. The sample panels were received at the Evaluation Center on June 22, and September 20, 2018.

#### **SECTION 4**

#### SAMPLE ASSEMBLY AND DESCRIPTION

Upon receipt of the samples at the Intertek Coquitlam laboratory they were placed in a conditioning room where they remained in an atmosphere of  $23 \pm 3^{\circ}$ C ( $73.4 \pm 5^{\circ}$ F) and  $50 \pm 5\%$  relative humidity.

The product was identified as nominal 2 in. by 6 in. SPF NLT Panels (Parallel). Samples submitted for testing measured nominal 6 in thick by 23 in. wide by 6 ft. long.

For each trial run, Four, Nominal 6 in. thick by 23 in. wide by 6 ft. long sample decks were butted together end to end to form the required 24 ft. sample length and placed on the upper ledge of the flame spread tunnel. A layer of 6 mm reinforced cement board was placed over top of the samples, the tunnel lid was lowered into place, and the samples were then tested in accordance with CAN/ULC S102-18.

#### SECTION 5 TESTING AND EVALUATION METHODS

#### TEST STANDARD

The results of the tests are expressed by indexes, which compare the characteristics of the sample under tests relative to that of select grade red oak flooring and inorganic-cement board.

#### (A) Flame Spread Rating:

This index relates to the rate of progression of a flame along a sample in the 25 foot tunnel. A natural gas flame is applied to the front of the sample at the start of the test and drawn along the sample by a draft kept constant for the duration of the test. An observer notes the progression of the flame front relative to time.

The test apparatus is calibrated such that the flame front for red oak flooring passes out the end of the tunnel in five minutes, thirty seconds (plus or minus 15 seconds).

#### (B) Smoke Developed:

A photocell is used to measure the amount of light, which is obscured by the smoke passing down the tunnel duct. When the smoke from a burning sample obscures the light beam, the output from the photocell decreases. This decrease with time is recorded and compared to the results obtained for red oak, which is defined to be 100.

## SECTION 6 RESULTS AND OBSERVATIONS

#### (A) Flame Spread

The resultant flame spread ratings are as follows: (Rating rounded to nearest 5)

2 in. by 6 in. SPF NLT Panels (Parallel)	Flame Spread	Flame Spread Rating
Run 1	40	
Run 2	45	50
Run 3	69	

#### (B) Smoke Developed

The areas beneath the smoke developed curve and the related classifications are as follows: (Classification rounded to nearest 5)

2 in. by 6 in. SPF NLT Panels (Parallel)	Smoke Developed	Smoked Developed Classification
Run 1	19	
Run 2	50	40
Run 3	53	

#### (C) Observations

During the test runs, the surface ignited between 23 and 30 seconds. The flame then began to progress along the sample length until it reached the maximum flame spread. This was the case for all three test runs.

#### SECTION 7

#### CONCLUSION

The samples of nominal 2 in. by 6 in. SPF NLT Panels (Parallel), submitted by FP Innovations exhibited the following flame spread characteristics when tested in accordance CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

A series of three test runs of material was conducted to conform to the requirements of the National Building Code of Canada.

Sample Material	Flame Spread Rating	Smoke Developed Classification
2 in. by 6 in. SPF NLT Panels (Parallel)	50	40

The conclusions of this test report may not be used as part of the requirements for Intertek product certification. Authority to Mark must be issued for a product to become certified.

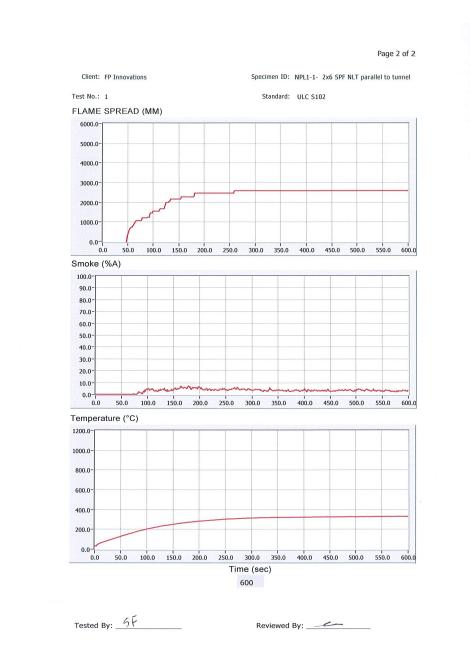
## TEST REPORT FOR FP INNOVATIONS

Revised October 19, 2018

## **SECTION 8**

**APPENDIX A: TEST DATA (6 PAGES)** 

Page 1 of 2 Standard: **ULC S102** Client: FP Innovations Date: 06 26 2018 Project Number: 103546754 Test Number: 1 Operator: Sean Fewer Specimen ID: NPL1-1- 2x6 SPF NLT parallel to tunnel TEST RESULTS FLAMESPREAD INDEX: 40 SMOKE DEVELOPED INDEX: 20 SPECIMEN DATA . . . Time to Ignition (sec): 23 Time to Max FS (sec): 264 Maximum FS (mm): 2596.0 Time to 527 C (sec): Never Reached Time to End of Tunnel (sec): Never Reached Max Temperature (C): 331 Time to Max Temperature (sec): 591 Total Fuel Burned (cubic feet): 45.70 FS\*Time Area (M\*min): 21.5 Smoke Area (%A\*min): 32.5 Unrounded FSI: 39.9 Unrounded SDI: 19.4 CALIBRATION DATA . . . Time to Ignition of Last Red Oak (Sec): 40.0 Red Oak Smoke Area (%A\*min): 167.5 Tested By: \_\_\_\_\_\_ Reviewed By:



Standard:

ULC S102

Page 1 of 2

Client: FP Innovations Date: 06 26 2018 Project Number: 103546754 Test Number: & 3 /m Operator: Sean Fewer

Specimen ID: NPPL3-3 SPF NLT parallel to tunnel

#### TEST RESULTS

FLAMESPREAD INDEX: 45 SMOKE DEVELOPED INDEX: 50

SPECIMEN DATA . . .

Time to Ignition (sec): 30 Time to Max FS (sec): 313 Maximum FS (mm): 3105.5 Time to 527 C (sec): Never Reached Time to End of Tunnel (sec): Never Reached Max Temperature (C): 401 Time to Max Temperature (sec): 507 Total Fuel Burned (cubic feet): 45.70

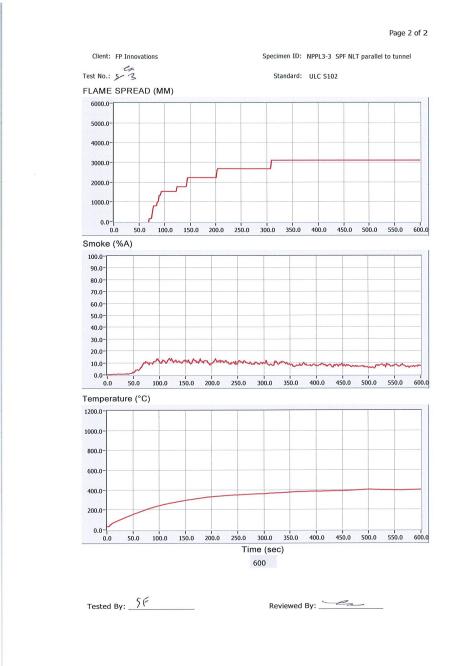
> FS\*Time Area (M\*min): 23.6 Smoke Area (%A\*min): 81.6 Unrounded FSI: 43.7 Unrounded SDI: 48.7

CALIBRATION DATA . . .

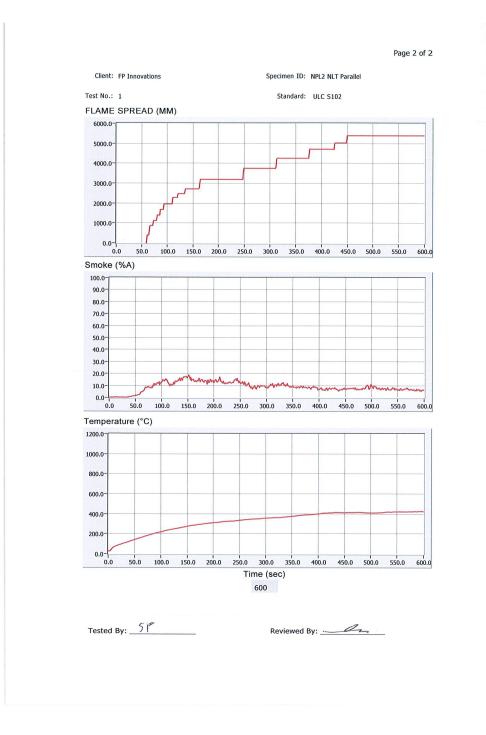
Time to Ignition of Last Red Oak (Sec): 40.0 Red Oak Smoke Area (%A\*min): 167.5

Tested By: \_\_\_\_\_

Reviewed By:



Standard:	ULC S	S102	Р	age 1 of 2	
Client: FP Inr Date: 09 25 Project Number: 10354 Test Number: 1 Operator: Sean	5 2018 46754				
Specimen ID: NPL2	NLT Parallel				
TEST RESULTS					
FLAM	ESPREAD INDEX:	70			
SMOKE DE	VELOPED INDEX:	55			
SPECIMEN DATA					
Tin	ne to Ignition (sec):	27			5
	e to Max FS (sec):				
	1aximum FS (mm):				
	me to 527 C (sec):				
	nd of Tunnel (sec):				
	κ Temperature (C): Γemperature (sec):				
	Burned (cubic feet):				
FS*T	ime Area (M*min)	35.8			
Smol	ke Area (%A*min):				
	Unrounded FSI: Unrounded SDI:				
CALIBRATION DATA					
Time to Ignition of Las	at Red Oak (Sec):	40.0			
	e Area (%A*min):				
Tested By: 5F			Reviewed By:		
	<u>x 3</u> -				



#### **REVISION SUMMARY**

DATE	PAGE	SUMMARY
September 26, 2018	All	Original Issue Date
October 19, 2018	6&7	Corrected Data

# Appendix II: NLT Perpendicular to Tunnel (B) Testing Report



# FP INNOVATIONS TEST REPORT

REPORT ISSUED TO FP Innovations 580 Booth Street Ottawa, ON K1A 0E4 CAN SCOPE OF WORK

Report of R&D testing nominal 2 in. by 6 in. SPF NLT Panels (Perpendicular) for compliance with the applicable requirements of the following criteria: CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

### **REPORT NUMBER**

103546754COQ-001d

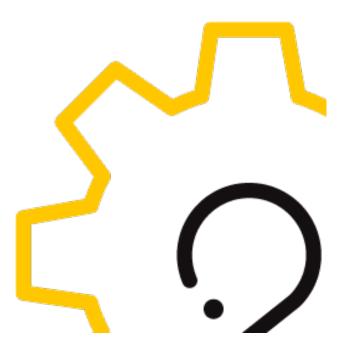
**ISSUE DATE** 26-September-2018

PAGES

15

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**TEST REPORT FOR FP INNOVATIONS** REPORT NO.: G103546754

DATE: SEPTEMBER 26, 2018

# CONCLUSION

The samples of nominal 2 in. by 6 in. SPF NLT Panels (Perpendicular) submitted by FP Innovations, were tested in accordance with CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

The product test results are presented in Section 7 of this report.

Sean Fewer **TECHNICIAN BUILDING PRODUCTS** 

Thile Greg Philp

REVIEWER **BUILDING PRODUCTS CANADA** 

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## INDEX

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Testing and Evaluation Methods	5
Results and Observations	6
Conclusion	7
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REVISION SUMMARY	

# SECTION 2

## OBJECTIVE

Intertek Testing Services NA Ltd. (Intertek) has conducted testing for FP Innovations to evaluate the surface burning characteristics of 2 in. by 6 in. SPF NLT Panels (Perpendicular). Testing was conducted in accordance with the standard methods of CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

This evaluation began June 26, 2018 and was completed September 25, 2018.

## SECTION 3

## SAMPLE SELECTION

Samples were submitted to Intertek directly from the client and were not independently selected for testing. The sample panels were received at the Evaluation Center on June 22, and September 20, 2018.

## **SECTION 4**

## SAMPLE ASSEMBLY AND DESCRIPTION

Upon receipt of the samples at the Intertek Coquitlam laboratory they were placed in a conditioning room where they remained in an atmosphere of  $23 \pm 3^{\circ}$ C ( $73.4 \pm 5^{\circ}$ F) and  $50 \pm 5\%$  relative humidity.

The product was identified as nominal 2 in. by 6 in. SPF NLT Panels (Perpendicular). Samples submitted for testing measured nominal 6 in thick by 23 in. wide by 6 ft. long.

For each trial run, Four, Nominal 6 in. thick by 23 in. wide by 6 ft. long sample decks were butted together end to end to form the required 24 ft. sample length and placed on the upper ledge of the flame spread tunnel. A layer of 6 mm reinforced cement board was placed over top of the samples, the tunnel lid was lowered into place, and the samples were then tested in accordance with CAN/ULC S102-18.

## SECTION 5 TESTING AND EVALUATION METHODS

### TEST STANDARD

The results of the tests are expressed by indexes, which compare the characteristics of the sample under tests relative to that of select grade red oak flooring and inorganic-cement board.

### (A) Flame Spread Rating:

This index relates to the rate of progression of a flame along a sample in the 25 foot tunnel. A natural gas flame is applied to the front of the sample at the start of the test and drawn along the sample by a draft kept constant for the duration of the test. An observer notes the progression of the flame front relative to time.

The test apparatus is calibrated such that the flame front for red oak flooring passes out the end of the tunnel in five minutes, thirty seconds (plus or minus 15 seconds).

### (B) Smoke Developed:

A photocell is used to measure the amount of light, which is obscured by the smoke passing down the tunnel duct. When the smoke from a burning sample obscures the light beam, the output from the photocell decreases. This decrease with time is recorded and compared to the results obtained for red oak, which is defined to be 100.

# SECTION 6 RESULTS AND OBSERVATIONS

#### (A) Flame Spread

The resultant flame spread ratings are as follows: (Rating rounded to nearest 5)

2 in. by 6 in. SPF NLT Panels (Perpendicular)	Flame Spread	Flame Spread Rating
Run 1	35	
Run 2*	47	45
Run 3	55	

\*Due to a program error, flame spread data was not collected. Flame Spread Values were manually calculated

#### (B) Smoke Developed

The areas beneath the smoke developed curve and the related classifications are as follows: (Classification rounded to nearest 5)

2 in. by 6 in. SPF NLT Panels (Perpendicular)	Smoke Developed	Smoked Developed Classification
Run 1	72	
Run 2	*	55
Run 3	40	

\*Due to a program error, smoke value data was not collected. The Average is based on the two tests

#### (C) Observations

During the test runs, the surface ignited between 26 and 34 seconds. The flame then began to progress along the sample length until it reached the maximum flame spread. This was the case for all three test runs.

### **SECTION 7**

## CONCLUSION

The samples of nominal 2 in. by 6 in. SPF NLT Panels (Perpendicular), submitted by FP Innovations exhibited the following flame spread characteristics when tested in accordance CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

A series of three test runs of material was conducted to conform to the requirements of the National Building Code of Canada.

Sample Material	Flame Spread Rating	Smoke Developed Classification
2 in. by 6 in. SPF NLT Panels (Perpendicular)	45	55

The conclusions of this test report may not be used as part of the requirements for Intertek product certification. Authority to Mark must be issued for a product to become certified.

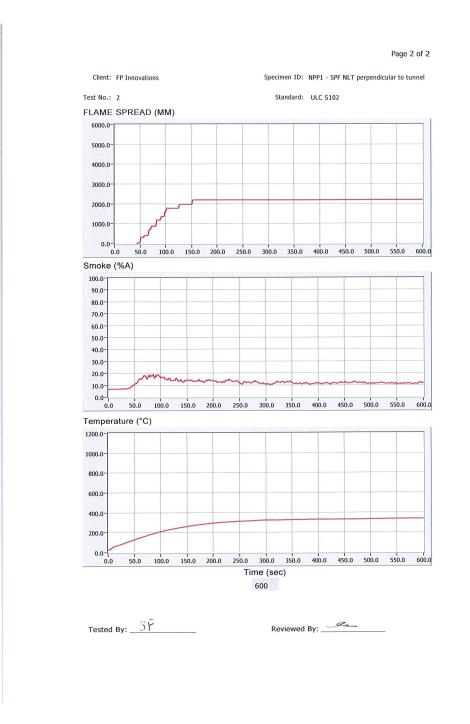
# TEST REPORT FOR FP INNOVATIONS

September 26, 2018

# SECTION 8

**APPENDIX A: TEST DATA (6 PAGES)** 

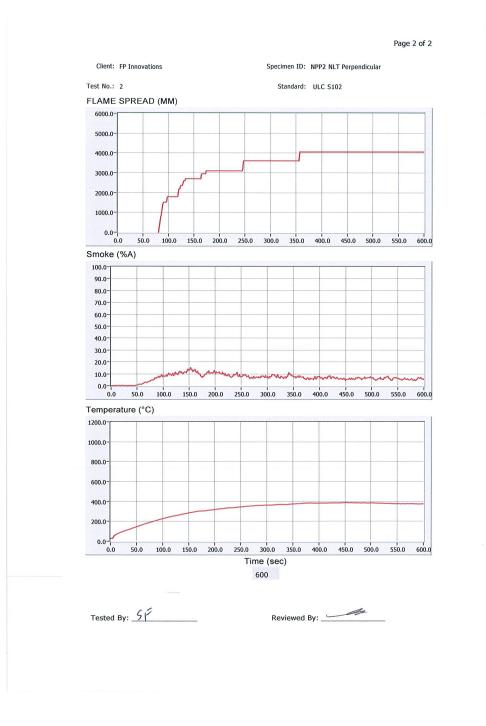
Star	ndard:	ULC S	6102		Page 1 of 2	
	Client: FP Date: 06 Project Number: 103 Test Number: 2 Operator: Sea	26 2018 3546754				
	Specimen ID: NPI	P1 - SPF NLT perpendi	icular to tunnel			
TEST	T RESULTS					
	FLA	MESPREAD INDEX:	35			
	SMOKE	DEVELOPED INDEX:	70			
SPEC	CIMEN DATA					
	T Time to M Time to Ma Total Fue FS	Fime to Ignition (sec): ime to Max FS (sec): Maximum FS (mm): Time to 527 C (sec): End of Tunnel (sec): Ax Temperature (C): x Temperature (sec): I Burned (cubic feet): Burned (cubic feet): Time Area (%A*min): Unrounded FSI: Unrounded SDI:	157 2189.9 Never Reached 337 583 45.70 18.6 120.9 34.5			
CALII	BRATION DATA					
		ast Red Oak (Sec): oke Area (%A*min):				
Te	sted By:			Reviewed By:		



Data Lost Due To Program Error

Data Lost Due To Program Error

Standard:	ULC S	6102		Page 1 of 2
Client: FP In Date: 09 2 Project Number: 1035 Test Number: 2 Operator: Sean	5 2018 46754			
Specimen ID: NPP2	NLT Perpendicular			
TEST RESULTS				
FLAM	ESPREAD INDEX:	55		
	EVELOPED INDEX:			
SPECIMEN DATA				
Ti	me to Ignition (sec):	34		
Tin	ne to Max FS (sec):	362		
	Maximum FS (mm):			
	ime to 527 C (sec):			
	End of Tunnel (sec):			
	x Temperature (C):			
	Temperature (sec):			
Total Fuel	Burned (cubic feet):	45.70		
ES*	Time Area (M*min):	30.2		
	oke Area (%A*min):			
	Unrounded FSI:			
	Unrounded SDI:	40.6		
CALIBRATION DATA				
Time to Ignition of La	st Red Oak (Sec):	40.0		
Red Oak Smol	ke Area (%A*min):	167.5		
Tested By: 5			Reviewed By:	



#### **REVISION SUMMARY**

DATE	PAGE	SUMMARY
September 26, 2018	All	Original Issue Date

Appendix III: NLT Fluted Parallel to Tunnel (C) Testing Report



# FP INNOVATIONS TEST REPORT

REPORT ISSUED TO FP Innovations 580 Booth Street Ottawa, ON K1A 0E4 CAN SCOPE OF WORK

Report of R&D testing nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel) for compliance with the applicable requirements of the following criteria: CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

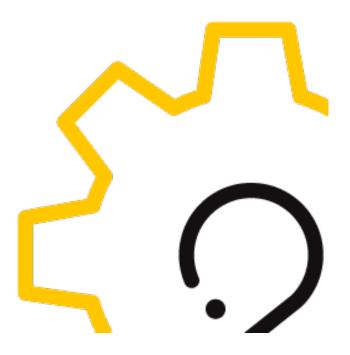
### **REPORT NUMBER**

103546754COQ-001e

### **ISSUE DATE**

26-September-2018 REVISION DATE 19-October-2018 PAGES 15

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**TEST REPORT FOR FP INNOVATIONS** REPORT NO.: G103546754

**REVISION DATE: OCTOBER 19, 2018** 

## CONCLUSION

The samples of 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel) submitted by FP Innovations, were tested in accordance with CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

The product test results are presented in Section 7 of this report.

Sean Fewer **TECHNICIAN BUILDING PRODUCTS** 

Thile Greg Philp

REVIEWER **BUILDING PRODUCTS CANADA** 

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### **TEST REPORT FOR FP INNOVATIONS** Revised October 19, 2018

## **SECTION 1**

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## **SECTION 2**

## OBJECTIVE

Intertek Testing Services NA Ltd. (Intertek) has conducted testing for FP Innovations to evaluate the surface burning characteristics of nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel). Testing was conducted in accordance with the standard methods of CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

This evaluation began June 26, 2018 and was completed September 26, 2018.

## SECTION 3

## SAMPLE SELECTION

Samples were submitted to Intertek directly from the client and were not independently selected for testing. The sample panels were received at the Evaluation Center on June 22, and September 20, 2018.

## **SECTION 4**

## SAMPLE ASSEMBLY AND DESCRIPTION

Upon receipt of the samples at the Intertek Coquitlam laboratory they were placed in a conditioning room where they remained in an atmosphere of  $23 \pm 3^{\circ}$ C ( $73.4 \pm 5^{\circ}$ F) and  $50 \pm 5\%$  relative humidity.

The product was identified as nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel). Samples submitted for testing measured nominal 6 in thick by 23 in. wide by 6 ft. long.

For each trial run, Four, Nominal 6 in. thick by 23 in. wide by 6 ft. long sample decks were butted together end to end to form the required 24 ft. sample length and placed on the upper ledge of the flame spread tunnel. A layer of 6 mm reinforced cement board was placed over top of the samples, the tunnel lid was lowered into place, and the samples were then tested in accordance with CAN/ULC S102-18.

## SECTION 5 TESTING AND EVALUATION METHODS

### TEST STANDARD

The results of the tests are expressed by indexes, which compare the characteristics of the sample under tests relative to that of select grade red oak flooring and inorganic-cement board.

### (A) Flame Spread Rating:

This index relates to the rate of progression of a flame along a sample in the 25 foot tunnel. A natural gas flame is applied to the front of the sample at the start of the test and drawn along the sample by a draft kept constant for the duration of the test. An observer notes the progression of the flame front relative to time.

The test apparatus is calibrated such that the flame front for red oak flooring passes out the end of the tunnel in five minutes, thirty seconds (plus or minus 15 seconds).

### (B) Smoke Developed:

A photocell is used to measure the amount of light, which is obscured by the smoke passing down the tunnel duct. When the smoke from a burning sample obscures the light beam, the output from the photocell decreases. This decrease with time is recorded and compared to the results obtained for red oak, which is defined to be 100.

# SECTION 6 RESULTS AND OBSERVATIONS

#### (A) Flame Spread

The resultant flame spread ratings are as follows: (Rating rounded to nearest 5)

2 in. by 6 in. and 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel)	Flame Spread	Flame Spread Rating
Run 1	90	
Run 2	84	91
Run 3	99	

#### (B) Smoke Developed

The areas beneath the smoke developed curve and the related classifications are as follows: (Classification rounded to nearest 5)

2 in. by 6 in. and 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel)	Smoke Developed	Smoked Developed Classification
Run 1	67	
Run 2	153	105
Run 3	100	

#### (C) Observations

During the test runs, the surface ignited between 22 and 29 seconds. The flame then began to progress along the sample length until it reached the maximum flame spread. This was the case for all three test runs.

## **SECTION 7**

## CONCLUSION

The samples of nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel) submitted by FP Innovations exhibited the following flame spread characteristics when tested in accordance CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

A series of three test runs of material was conducted to conform to the requirements of the National Building Code of Canada.

Sample Material	Flame Spread Rating	Smoke Developed Classification
2 in. by 6 in. and 2 in. by 4 in. alternating depth SPF NLT Panels (Parallel)	80	120

The conclusions of this test report may not be used as part of the requirements for Intertek product certification. Authority to Mark must be issued for a product to become certified.

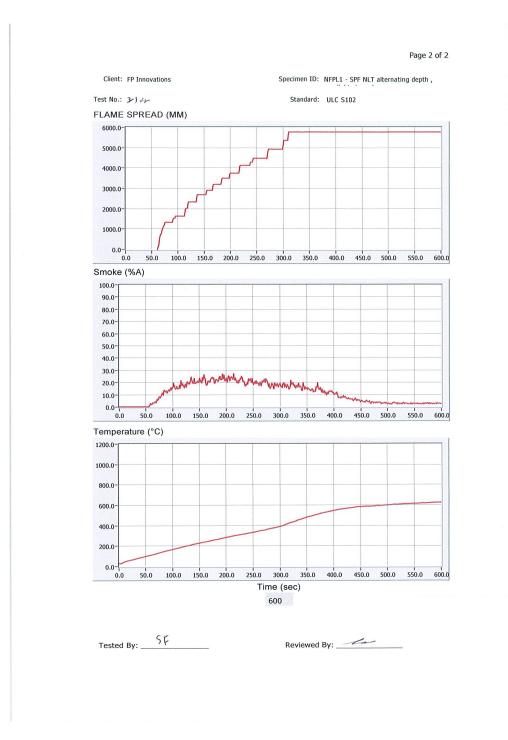
# TEST REPORT FOR FP INNOVATIONS

Revised October 19, 2018

# SECTION 8

**APPENDIX A: TEST DATA (6 PAGES)** 

Standard:	ULC S102	Page 1 of 2
Client: FF	P Innovations	
Date: 06	26 2018	
Project Number: 10		
Test Number: 3		
Operator: Se	an Fewer	
Specimen ID: NF	FPL1 - SPF NLT alternating depth , parallel to t	tunnel
TEST RESULTS		
FL	AMESPREAD INDEX: 90	
SMOKE	DEVELOPED INDEX: 65	
SPECIMEN DATA		
SPECIMEN DATA		
	Time to Ignition (sec): 27	
3	Time to Max FS (sec): 315	
	Maximum FS (mm): 5775.7	
	Time to 527C (sec): 385	
Time	to End of Tunnel (sec): 318	
	Max Temperature (C): 625	
	ax Temperature (sec): 593	
	el Burned (cubic feet): 45.70	
F	S*Time Area (M*min): 41.3	
S	moke Area (%A*min): 112.9	
	Unrounded FSI: 90.1	
	Unrounded SDI: 67.4	
CALIBRATION DATA		
Time to Ignition of	Least Dad Oak (Sea): 40.0	
-	Last Red Oak (Sec): 40.0	
Red Oak Sn	noke Area (%A*min): 167.5	
Tested By: 56	- 	La La
Tested By: 71	Re	eviewed By:



Standard:

ULC S102

Page 1 of 2

Client: FP Innovations Date: 06 26 2018 Project Number: 103546754 Test Number: <sup>-6' 3</sup> -> Operator: Sean Fewer

Specimen ID: NFPL3-3 SPF NLT alternating depth , parallel to tunnel

#### TEST RESULTS

FLAMESPREAD INDEX: 85 SMOKE DEVELOPED INDEX: 155

SPECIMEN DATA . . .

Time to Ignition (sec):25Time to Max FS (sec):331Maximum FS (mm):5783.2Time to 527C (sec):369Time to End of Tunnel (sec):326Max Temperature (C):620Time to Max Temperature (sec):598Total Fuel Burned (cubic feet):45.70

FS\*Time Area (M\*min): 39.9 Smoke Area (%A\*min): 255.8 Unrounded FSI: 83.8 Unrounded SDI: 152.7

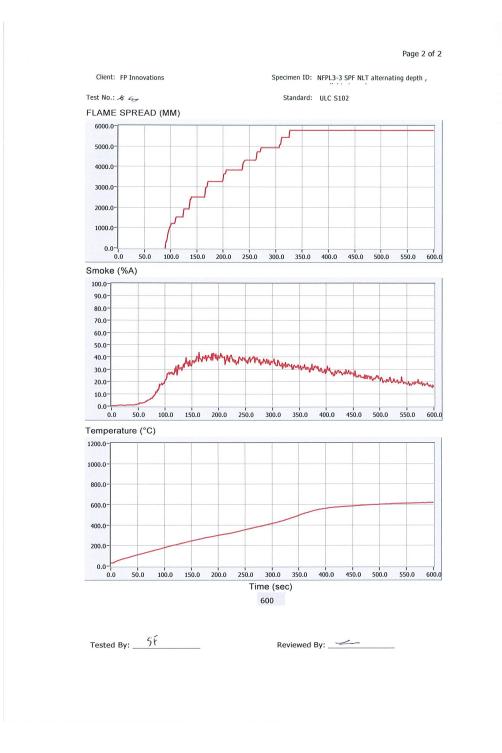
CALIBRATION DATA . . .

Time to Ignition of Last Red Oak (Sec): 40.0 Red Oak Smoke Area (%A\*min): 167.5

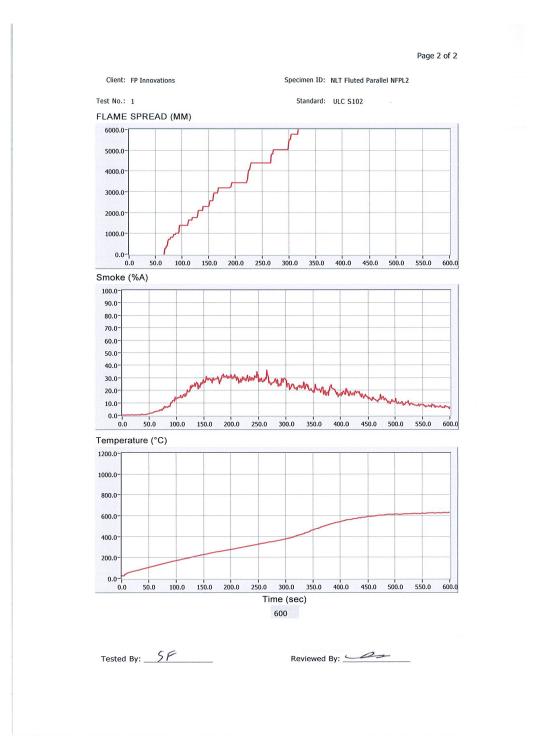
Tested By:  $\underline{5F}$ 

Version (13-March-2017)

Reviewed By:



FLAMESPREAD INDEX: 100 SMOKE DEVELOPED INDEX: 100 SPECIMEN DATA Time to Ignition (sec): 29 Time to Max FS (sec): 322 Maximum FS (mm): 6258.7 Time to 527C (sec): 389 Time to End of Tunnel (sec): 328 Max Temperature (Sec): 328 Time to Max Temperature (Sec): 589 Total Fuel Burned (cubic feet): 45.70 FS*Time Area (M*min): 42.8 Smoke Area (%A*min): 167.0 Unrounded FSI: 98.7 Unrounded SDI: 99.7	Standard:	ULC \$102	Page 1 of 2	
Late: 09 26 2018 Project Number: 103546754 Test Number: 1 Derator: Sean Fewer Specimen ID: NLT Fluted Parallel NFPL2 TEST RESULTS FLAMESPREAD INDEX: 100 SMOKE DEVELOPED INDEX: 100 SPECIMEN DATA Time to Ignition (sec): 29 Time to Max FS (sec): 322 Maximum FS (mm): 6258.7 Time to Max FS (sec): 322 Maximum FS (mm): 6258.7 Time to SZ7C (sec): 389 Time to End of Tunnel (sec): 328 Max Temperature (C): 629 Time to Max Temperature (Sec): 589 Total Fuel Burned (cubic feel): 45.70 ES*Time Area (M*min): 42.8 Smoke Area (M*min): 167.0 Unrounded FSI: 86.7 Unrounded SDI: 99.7	Client: F	P Innovations		
Project Number: 103546754 Test Number: 1 Operator: Sean Fewer Specimen ID: NLT Fluted Parallel NFPL2 TEST RESULTS FLAMESPREAD INDEX: 100 SMOKE DEVELOPED INDEX: 100 SPECIMEN DATA Time to Ignition (sec): 29 Time to Max FS (sec): 322 Maximum FS (mm): 6258.7 Time to Max FS (sec): 322 Maximum FS (mm): 6258.7 Time to Max Temperature (SC): 639 Time to Max Temperature (SC): 639 Total Fuel Burned (cubic feet): 45.70 ES*Time Area (M*min): 42.8 Smoke Area (%A*min): 167.0 Unrounded FSI: 98.7 Unrounded FSI: 98.7 Unrounded FSI: 98.7				
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Operator:       Sean Fewer         Specimen ID:       NLT Fluted Parallel NFPL2         TEST RESULTS       FLAMESPREAD INDEX:       100         SPECIMEN DATA       SPECIMEN DATA         SPECIMEN DATA       Time to Ignition (sec):       29         Time to Ignition (sec):       29         Maximum FS (sec):       322         Maximum FS (sec):       322         Maximum FS (sec):       328         Max Temperature (sec):       328         Max Temperature (sec):       328         Time to Max Temperature (sec):       598         Total Fuel Burned (cubic feel):       45.70         Est Time Area (M*min):       42.8         Smoke Area (%A*min):       59.7         Unrounded FSI:       99.7         CALIBRATION DATA       Time to Ignition of Last Red Oak (Sec):         Yen to Ignition of Last Red Oak (Sec):       40.6				
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	Time to Ignition of	of Last Red Oak (Sec): 40.0		



### **TEST REPORT FOR FP INNOVATIONS** Revised October 19, 2018

#### **REVISION SUMMARY**

DATE	PAGE	SUMMARY
September 26, 2018	All	Original Issue Date
October 19, 2018	6&7	Corrected Data

Appendix IV: NLT Fluted Perpendicular to Tunnel (D) Testing Report



# FP INNOVATIONS TEST REPORT

REPORT ISSUED TO FP Innovations 580 Booth Street Ottawa, ON K1A 0E4 CAN SCOPE OF WORK

Report of R&D testing nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular) for compliance with the applicable requirements of the following criteria: CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

### **REPORT NUMBER**

103546754COQ-001f

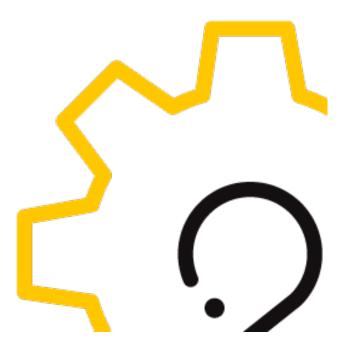
**ISSUE DATE** 26-September-2018

PAGES

15

#### DOCUMENT CONTROL NUMBER

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**TEST REPORT FOR FP INNOVATIONS** REPORT NO.: G103546754

DATE: SEPTEMBER 26, 2018

## CONCLUSION

The samples of 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular) submitted by FP Innovations, were tested in accordance with CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

The product test results are presented in Section 7 of this report.

Sean Fewer **TECHNICIAN BUILDING PRODUCTS** 

Thile Greg Philp

REVIEWER **BUILDING PRODUCTS CANADA** 

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#### **SECTION 1**

### INDEX

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Sample and Assembly Description	4
Testing and Evaluation Methods	5
Results and Observations	6
Conclusion	7
APPENDEX –A TEST DATA	6 Pages
REVISION SUMMARY	

#### **SECTION 2**

### OBJECTIVE

Intertek Testing Services NA Ltd. (Intertek) has conducted testing for FP Innovations to evaluate the surface burning characteristics of nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular). Testing was conducted in accordance with the standard methods of CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

This evaluation began June 26, 2018 and was completed September 25, 2018.

#### SECTION 3

#### SAMPLE SELECTION

Samples were submitted to Intertek directly from the client and were not independently selected for testing. The sample panels were received at the Evaluation Center on June 22, and September 20, 2018.

#### **SECTION 4**

#### SAMPLE ASSEMBLY AND DESCRIPTION

Upon receipt of the samples at the Intertek Coquitlam laboratory they were placed in a conditioning room where they remained in an atmosphere of  $23 \pm 3^{\circ}$ C ( $73.4 \pm 5^{\circ}$ F) and  $50 \pm 5\%$  relative humidity.

The product was identified as nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular). Samples submitted for testing measured nominal 6 in thick by 23 in. wide by 6 ft. long.

For each trial run, Four, Nominal 6 in. thick by 23 in. wide by 6 ft. long sample decks were butted together end to end to form the required 24 ft. sample length and placed on the upper ledge of the flame spread tunnel. A layer of 6 mm reinforced cement board was placed over top of the samples, the tunnel lid was lowered into place, and the samples were then tested in accordance with CAN/ULC S102-18.

# SECTION 5 TESTING AND EVALUATION METHODS

#### TEST STANDARD

The results of the tests are expressed by indexes, which compare the characteristics of the sample under tests relative to that of select grade red oak flooring and inorganic-cement board.

#### (A) Flame Spread Rating:

This index relates to the rate of progression of a flame along a sample in the 25 foot tunnel. A natural gas flame is applied to the front of the sample at the start of the test and drawn along the sample by a draft kept constant for the duration of the test. An observer notes the progression of the flame front relative to time.

The test apparatus is calibrated such that the flame front for red oak flooring passes out the end of the tunnel in five minutes, thirty seconds (plus or minus 15 seconds).

#### (B) Smoke Developed:

A photocell is used to measure the amount of light, which is obscured by the smoke passing down the tunnel duct. When the smoke from a burning sample obscures the light beam, the output from the photocell decreases. This decrease with time is recorded and compared to the results obtained for red oak, which is defined to be 100.

# SECTION 6 RESULTS AND OBSERVATIONS

#### (A) Flame Spread

The resultant flame spread ratings are as follows: (Rating rounded to nearest 5)

2 in. by 6 in. and 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular)	Flame Spread	Flame Spread Rating	
Run 1	53		
Run 2	100	65	
Run 3	48		

#### (B) Smoke Developed

The areas beneath the smoke developed curve and the related classifications are as follows: (Classification rounded to nearest 5)

2 in. by 6 in. and 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular)	Smoke Developed	Smoked Developed Classification
Run 1	186	
Run 2	49	125
Run 3	147	

#### (C) Observations

During the test runs, the surface ignited between 22 and 28 seconds. The flame then began to progress along the sample length until it reached the maximum flame spread. This was the case for all three test runs.

## **SECTION 7**

### CONCLUSION

The samples of nominal 2 in. by 6 in. and nominal 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular) submitted by FP Innovations exhibited the following flame spread characteristics when tested in accordance CAN/ULC S102-18, Standard Method of Test for Surface Burning Characteristics of Building Materials and Assemblies.

A series of three test runs of material was conducted to conform to the requirements of the National Building Code of Canada.

Sample Material	Flame Spread Rating	Smoke Developed Classification
2 in. by 6 in. and 2 in. by 4 in. alternating depth SPF NLT Panels (Perpendicular)	65	125

The conclusions of this test report may not be used as part of the requirements for Intertek product certification. Authority to Mark must be issued for a product to become certified.

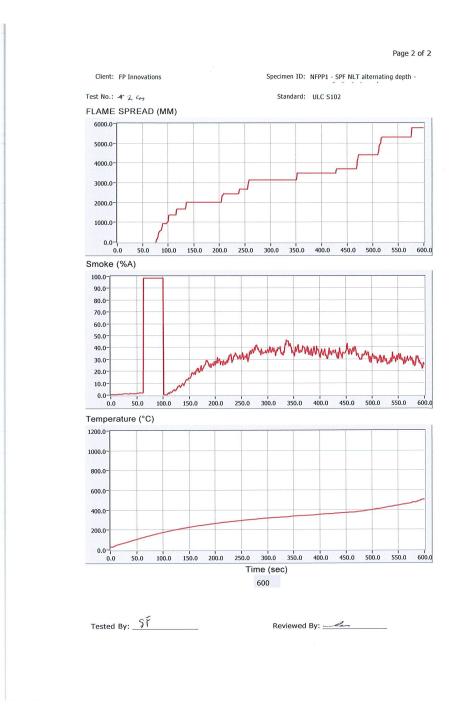
# TEST REPORT FOR FP INNOVATIONS

September 26, 2018

# SECTION 8

**APPENDIX A: TEST DATA (6 PAGES)** 

Standard:	ULC \$102		Page 1 of 2	
Client: F	P Innovations			
Date: (	06 26 2018			
Project Number:	103546754			
Test Number: 4	87 12			
Operator: \$				
Specimen ID: 1	NFPP1 - SPF NLT alternating depth - perpe	ndicular to tunnel		
TEST RESULTS				
	FLAMESPREAD INDEX: 55			
SMOK	E DEVELOPED INDEX: 185			
SPECIMEN DATA				
	Time to Ignition (sec): 22			
	Time to Max FS (sec): 582			
	Maximum FS (mm): 5782.1			
	Time to 527 C (sec): Never Reached			
Lim	e to End of Tunnel (sec): 580			
Time to	Max Temperature (C): 505			
	Max Temperature (sec): 598 Fuel Burned (cubic feet): 45.70			
Totarr	ruel Burried (cubic leet). 45.70			
	FS*Time Area (M*min): 28.6			
	Smoke Area (%A*min): 312.0			
	Unrounded FSI: 52.9 Unrounded SDI: 186.3			
	Unifoldaded 3D1, 160.5			
CALIBRATION DATA .				
Time to Ignition of	of Last Red Oak (Sec): 40.0			
	Smoke Area (%A*min): 167.5			
. /				
Tested By: 5r		Reviewed By:		



Standard:

#### ULC S102

Page 1 of 2

Client: FP Innovations Date: 09 25 2018 Project Number: 103546754 Test Number: 1 Operator: Sean Fewer

Specimen ID: NFPP2 NLT Fluted perpendicular

#### TEST RESULTS

# FLAMESPREAD INDEX: 100 SMOKE DEVELOPED INDEX: 50

SPECIMEN DATA . . .

Time to Ignition (sec):28Time to Max FS (sec):220Maximum FS (mm):5788.0Time to 527C (sec):289Time to End of Tunnel (sec):218Max Temperature (C):724Time to Max Temperature (sec):600Total Fuel Burned (cubic feet):45.70

FS\*Time Area (M\*min): 43.1 Smoke Area (%A\*min): 82.4 Unrounded FSI: 100.4 Unrounded SDI: 49.2

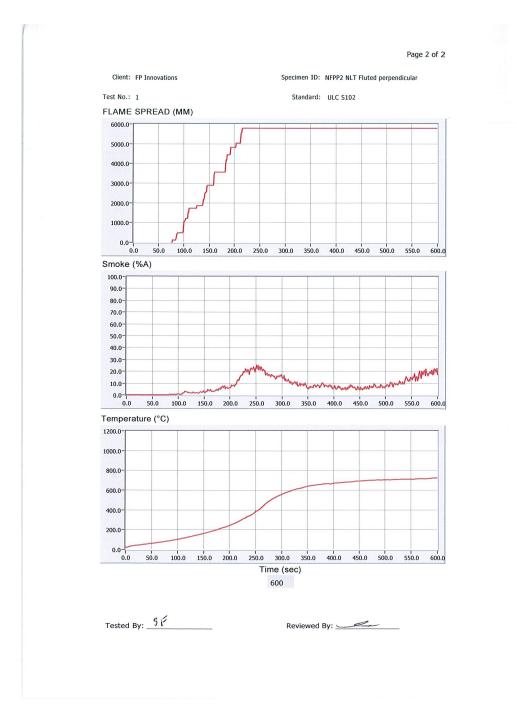
CALIBRATION DATA . . .

Time to Ignition of Last Red Oak (Sec): 40.0 Red Oak Smoke Area (%A\*min): 167.5

Tested By: SF

Reviewed By: S

02



Page 1 of 2

# CAN/ULC S102-18 DATA SHEETS Run 3

Standard:

ULC S102

Client: FP Innovations Date: 09 25 2018 Project Number: 103546754 Test Number: <sup>2</sup> Operator: Sean Fewer

Specimen ID: NFPP3 Fluted Perpendicular

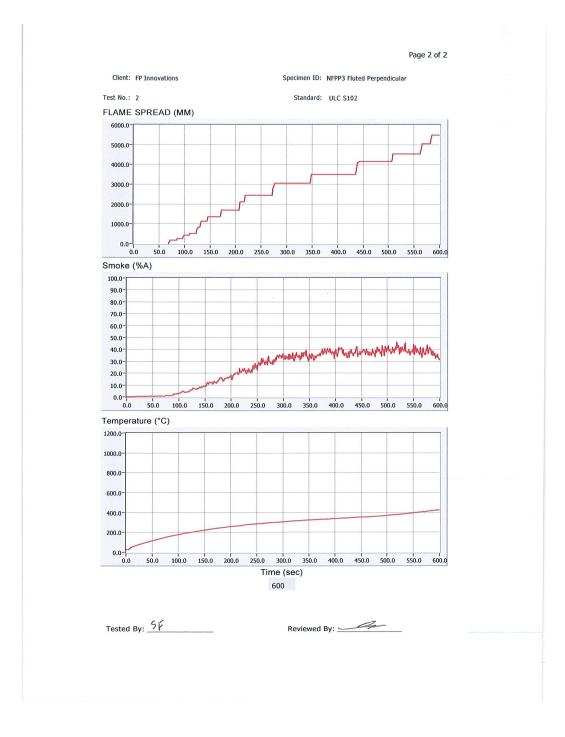
TEST RESULTS

FLAMESPREAD INDEX: 50

SMOKE DEVELOPED INDEX: 145

SPECIMEN DATA . . .

Time to Ignition (sec):	26
Time to Max FS (sec):	589
Maximum FS (mm):	5489.0
Time to 527 C (sec):	Never Reached
Time to End of Tunnel (sec):	Never Reached
Max Temperature (C):	424
Time to Max Temperature (sec):	
Total Fuel Burned (cubic feet):	
FS*Time Area (M*min):	26.1
Smoke Area (%A*min):	246.4
Unrounded FSI:	48.2
Unrounded SDI:	147.1
CALIBRATION DATA	
Time to Ignition of Last Red Oak (Sec):	40.0
Red Oak Smoke Area (%A*min):	167.5
Tested By: <u>SF</u>	Reviewed By:



#### **REVISION SUMMARY**

Version (13-March-2017)

DATE	PAGE	SUMMARY
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#### **OUR OFFICES**

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